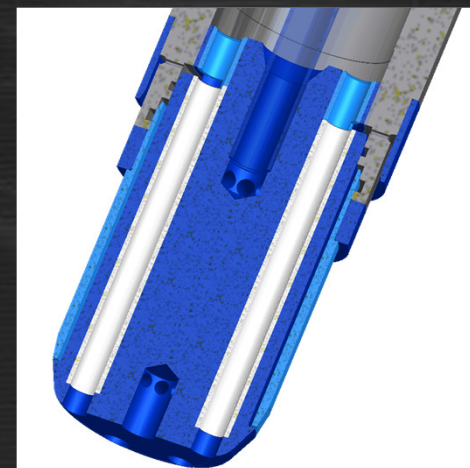
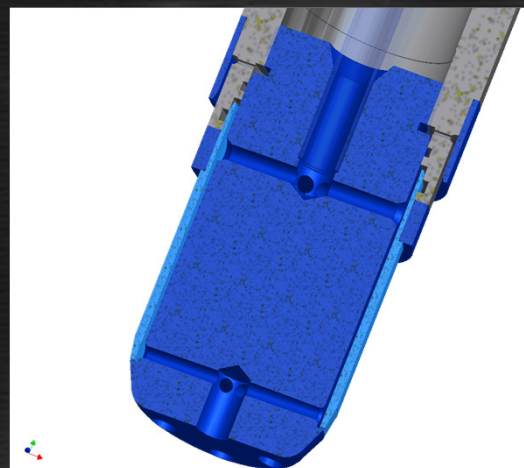
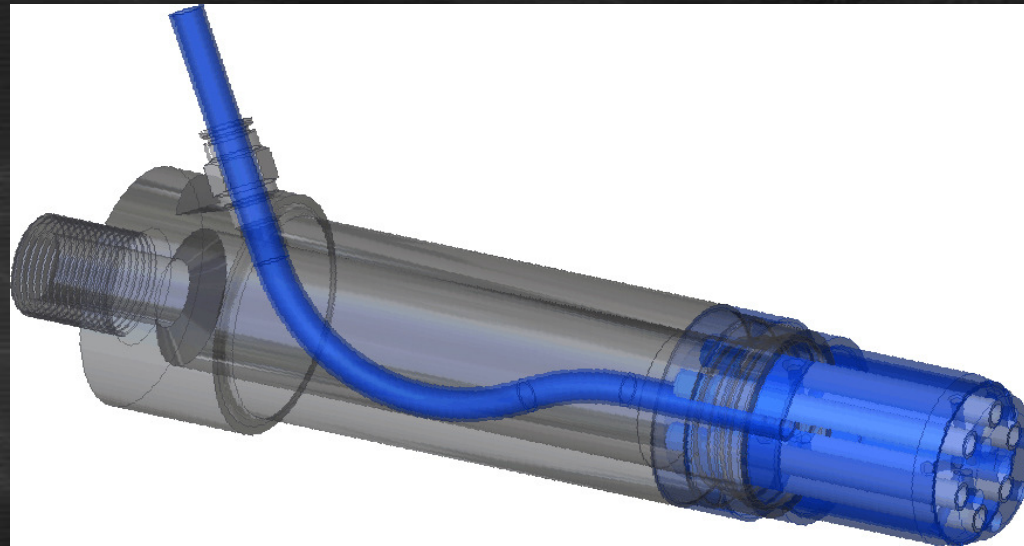
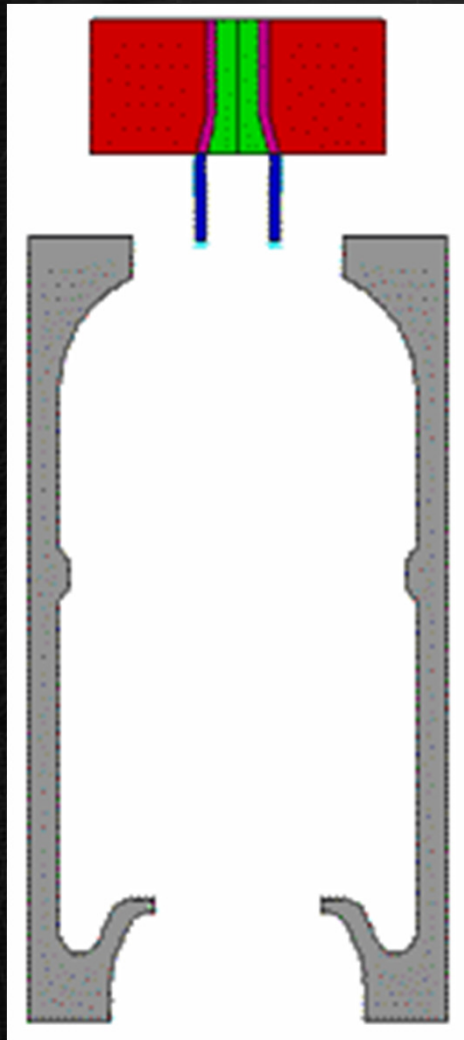


Heat transfer in blowmolding

Choise of the design

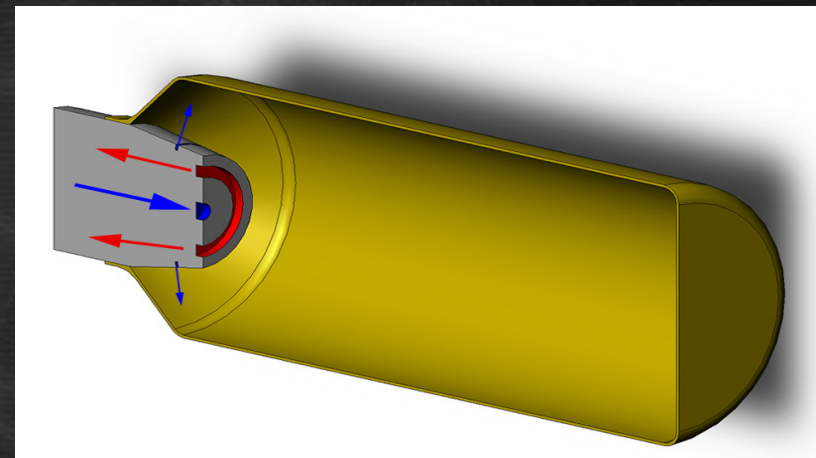


Choise of geometry

Actual blowthorn is replaced by a simplified geometry

Adjustments:

- Side inlets are replaced by a ring with same area.
- Outlet tubes are replaced by one ring with same area.



Grid

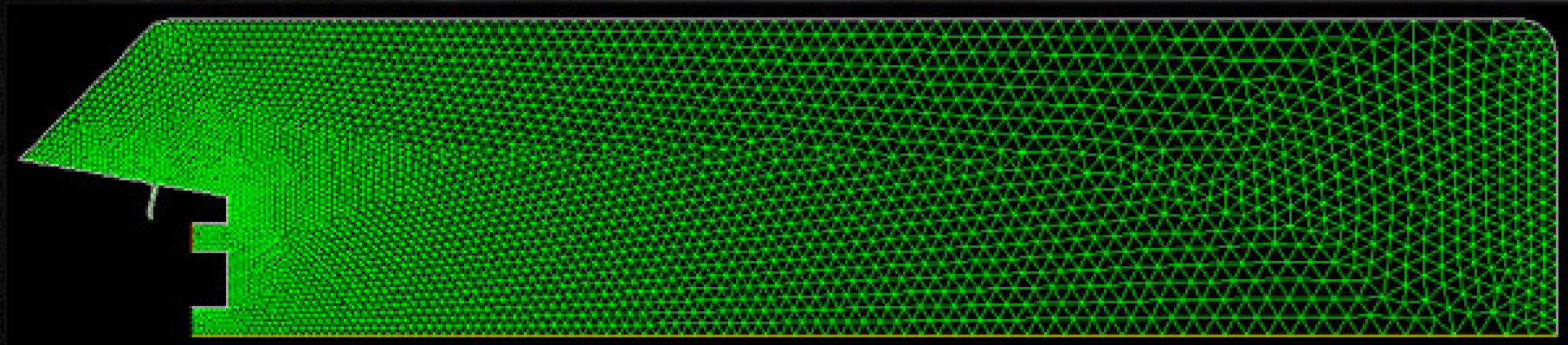
Node Distribution

- Most important areas
 - Inlets and outlets
 - Base –for distribution of the jet

Mesh specs:

- 2D Model (axisymmetric)
- Tri-elements
- Type: Pave
- started from: 7333 cells

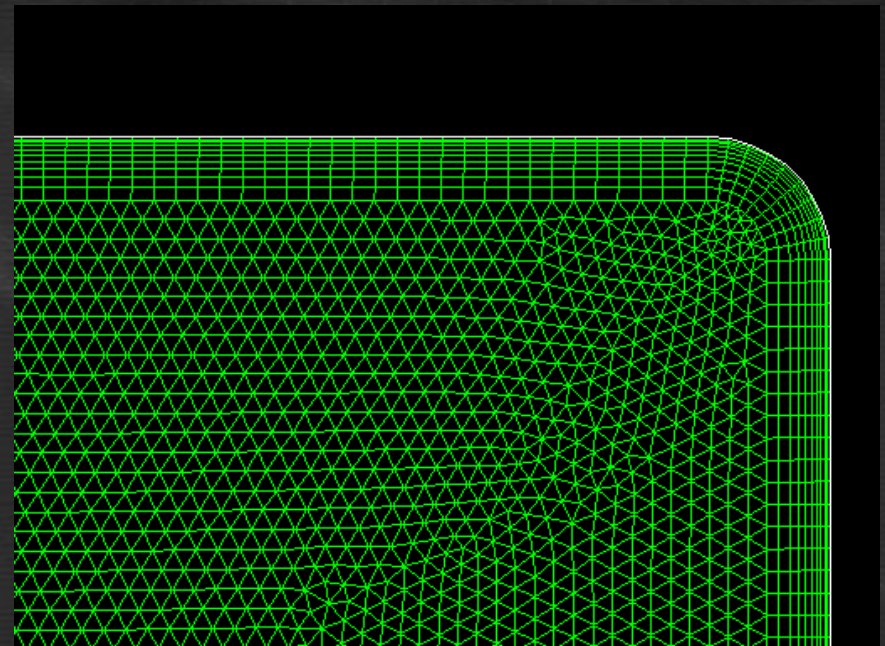
Double sided ratio op longest edges



Adjusted geometry

- Adjusted diameters of inlet and outlet
- Boundary layer added in combination with an unstructured mesh

(in order to get larger accuracy in the wall interaction with the air)



Setup

Solver:

- Pressure based: low speeds so the air can be assumed as quasi incompressible
- Gradient option: Green-Gauss Node Based
- Axisymmetric, Implicit, Steady
Energy Equation
- needed to calculate temperatures

Viscous Model:

- k- ϵ model (realizable)
- Also k- ϵ standard en k- ω SST calculated in one specific case

Boundary conditions

Conditions: volume flow rate chosen at 5,10,20 times the volume of the bottle

Operating conditions: 101325 Pa (1Atm)

Inlets:

- velocity-inlet
- Speed (using mass-law) is 62.3 m/s 126.6 m/s 253.13 m/s
- turbulence: intensity and hydraulic diameter
- Inlet Temperature: -35 °C, 4 °C en 30 °C

Outlet:

- Pressure-outlet
- 3 bar counterpressure (to atmosphere)
- turbulence: intensity and hydraulic diameter

$Q_{(m^3/s)}$ $T_{(°C)}$	0,0065	0,013	0,026
-35			
4			
30			

Boundary conditions (2)

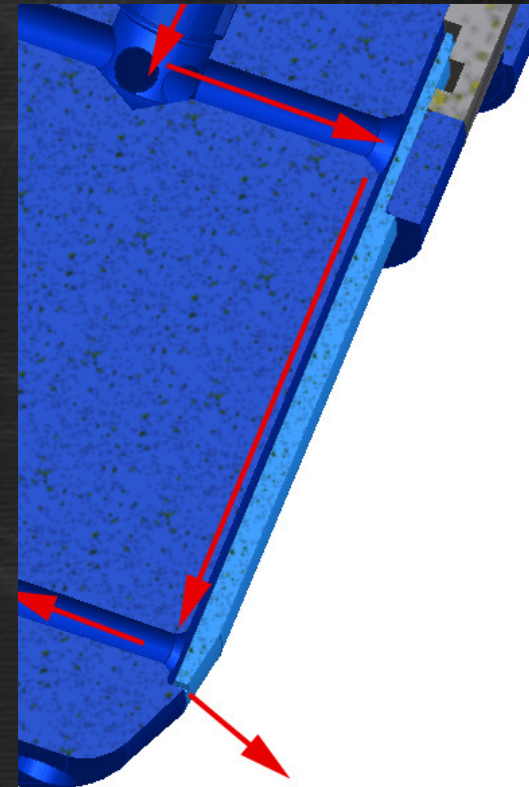
Wall of the bottle:

- Assumed at constant temperature of 473 K (PE just after production)

Thorn:

- Same temperature as incoming air

(chosen by the large area that comes in contact with the air in the actual situation)



Results

Temperature:

- At -35°C for the different flow rates
- At $0.0026\text{ m}^3/\text{s}$ on different temperatures

At largest flow rate, grid adaption is used in order to get correct Y^+ values)

(following is at $0.0026\text{ m}^3/\text{s}$ and -35°C Inlet temperature)

Contourplot

- Velocity magnitude \rightarrow flow rate almost no influence on path, only on magintude

Vectorplot: around the thorn

Heat Flux on the wall

K- ϵ (realizable – Standard) K- ω (SST)

Results

Temperature:

- At -35°C for the different flow rates
- At $0.0026\text{ m}^3/\text{s}$ on different temperatures

At largest flow rate, grid adaption is used in order to get correct Y_+ values)

(following is at $0.0026\text{ m}^3/\text{s}$ and -35°C Inlet temperature)

Contourplot

- Velocity magnitude \rightarrow flow rate almost no influence on path, only on magintude

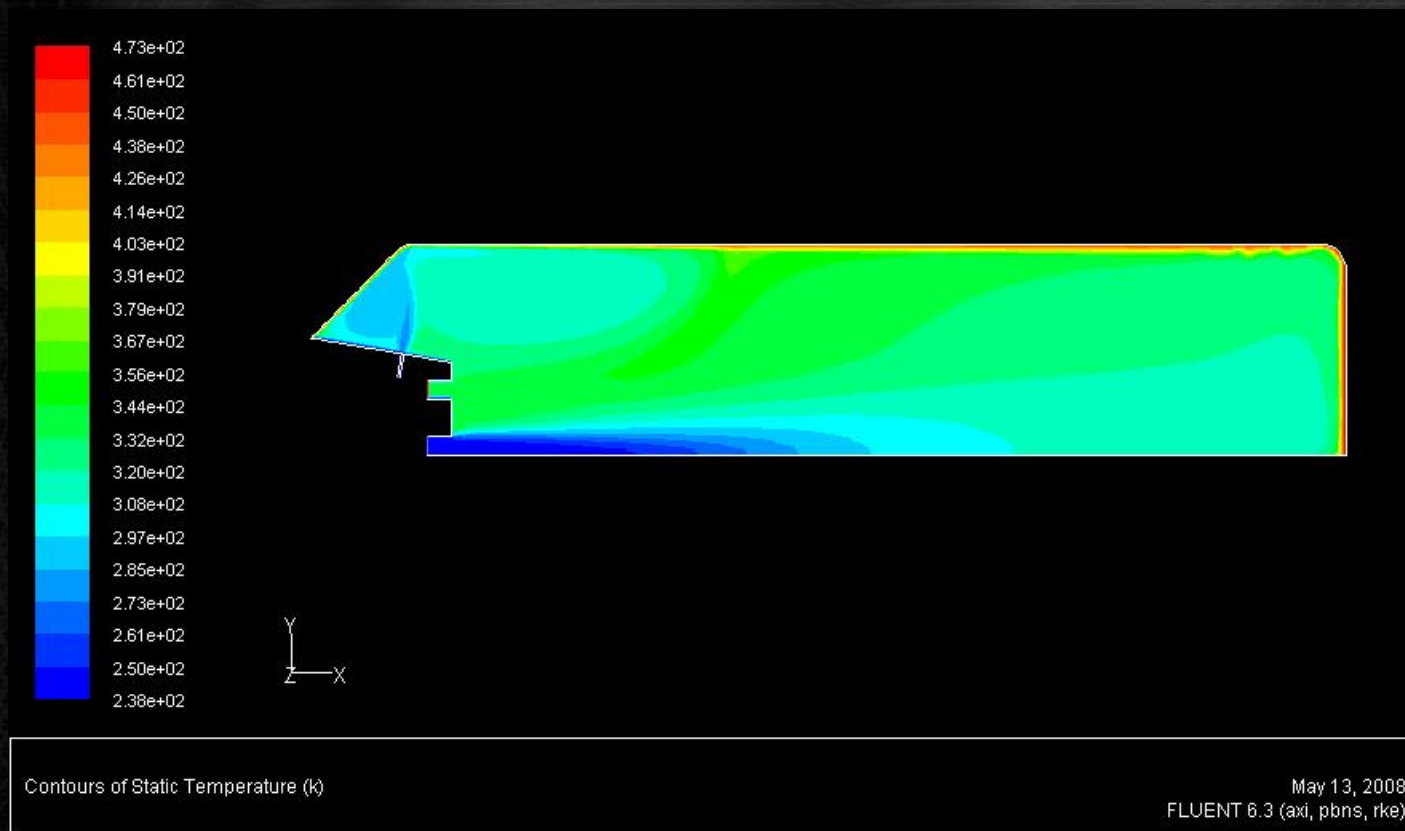
Vectorplot: around the thorn

Heat Flux on the wall

K- ϵ (realizable – Standard) K- ω (SST)

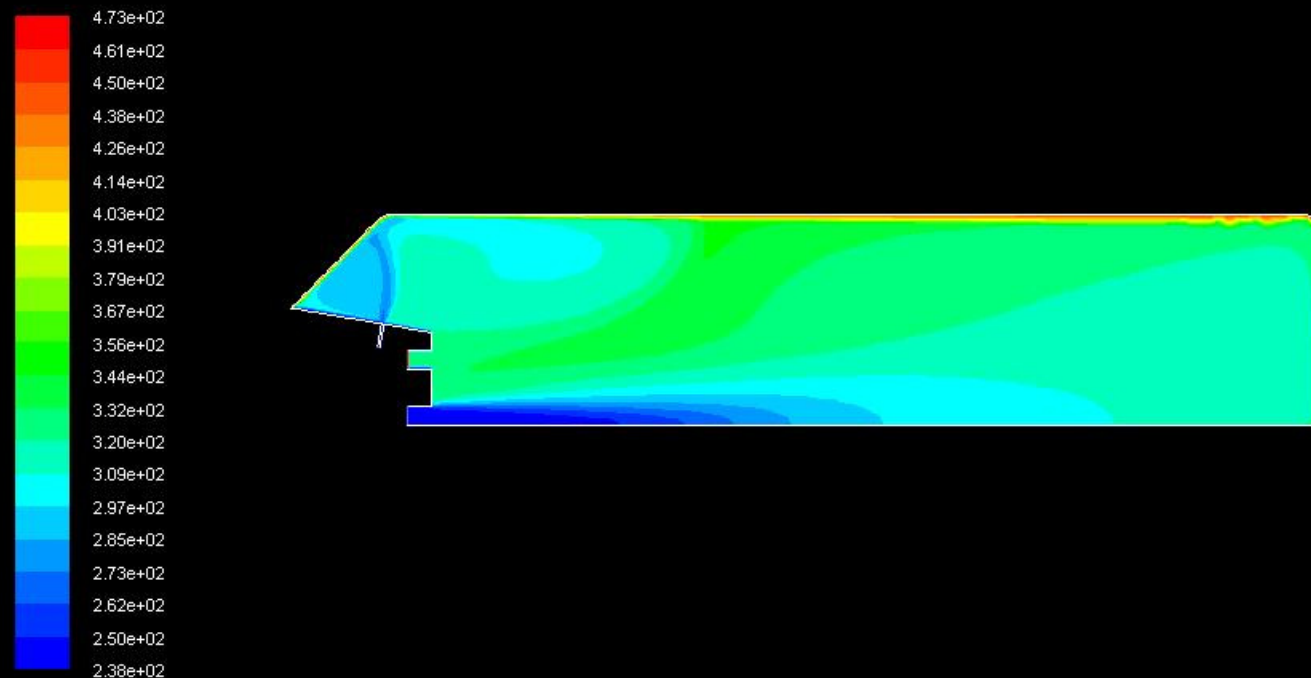
Static temperature 0.0065 m³/s

Temperatuur outlet: 64,7°C



Static temperature 0.013 m³/s

Temperatuur outlet: 53 °C

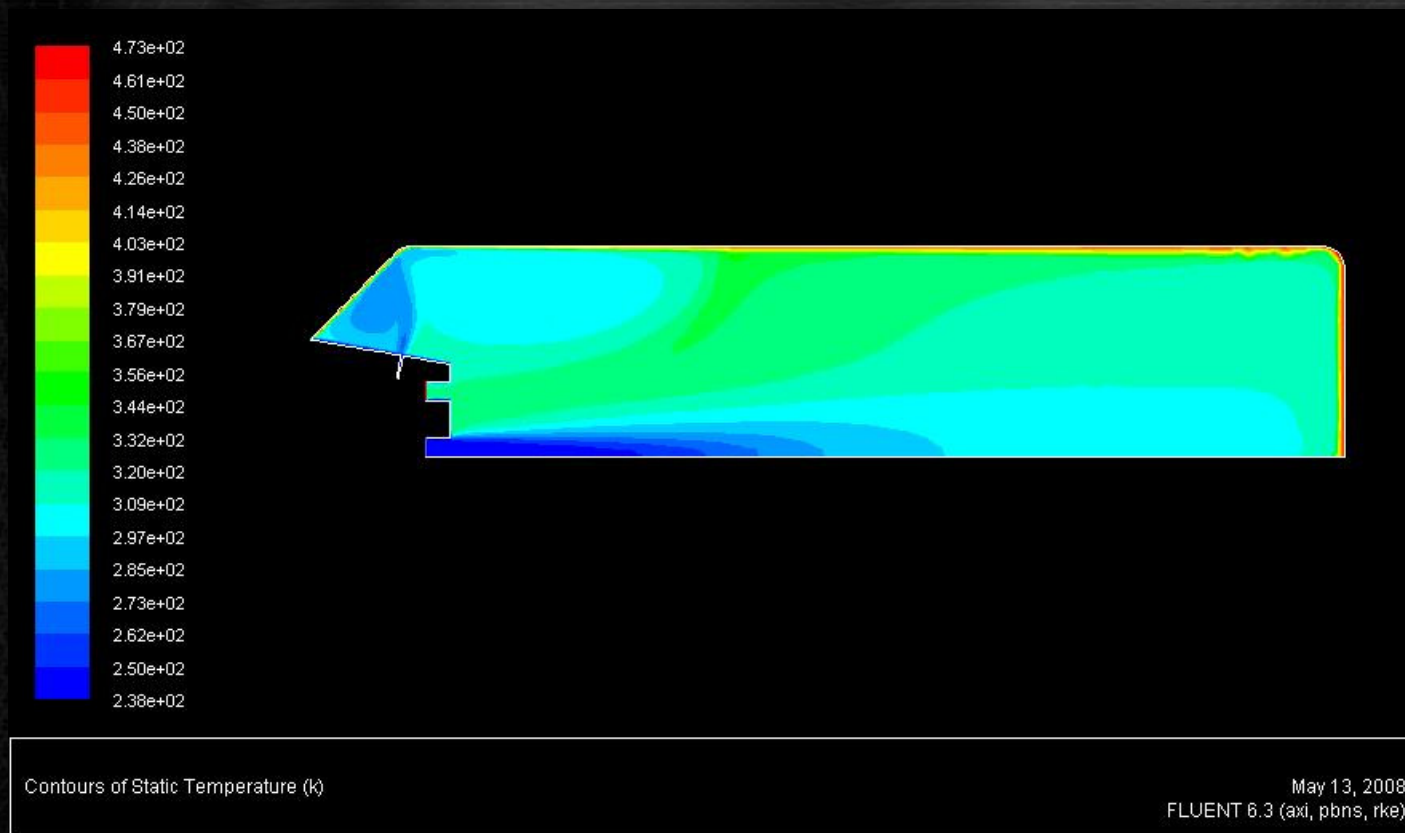


Contours of Static Temperature (K)

May 13, 2008
FLUENT 6.3 (axi, pbns, rke)

Static temperature 0.026 m³/s

Temperatuur outlet: 47,3°C



Results

Temperature:

- At -35°C for the different flow rates
- At $0.0026 \text{ m}^3/\text{s}$ on different temperatures

At largest flow rate, grid adaption is used in order to get correct Y^+ values)

(following is at $0.0026 \text{ m}^3/\text{s}$ and -35°C Inlet temperature)

Contourplot

- Velocity magnitude \rightarrow flow rate almost no influence on path, only on magintude

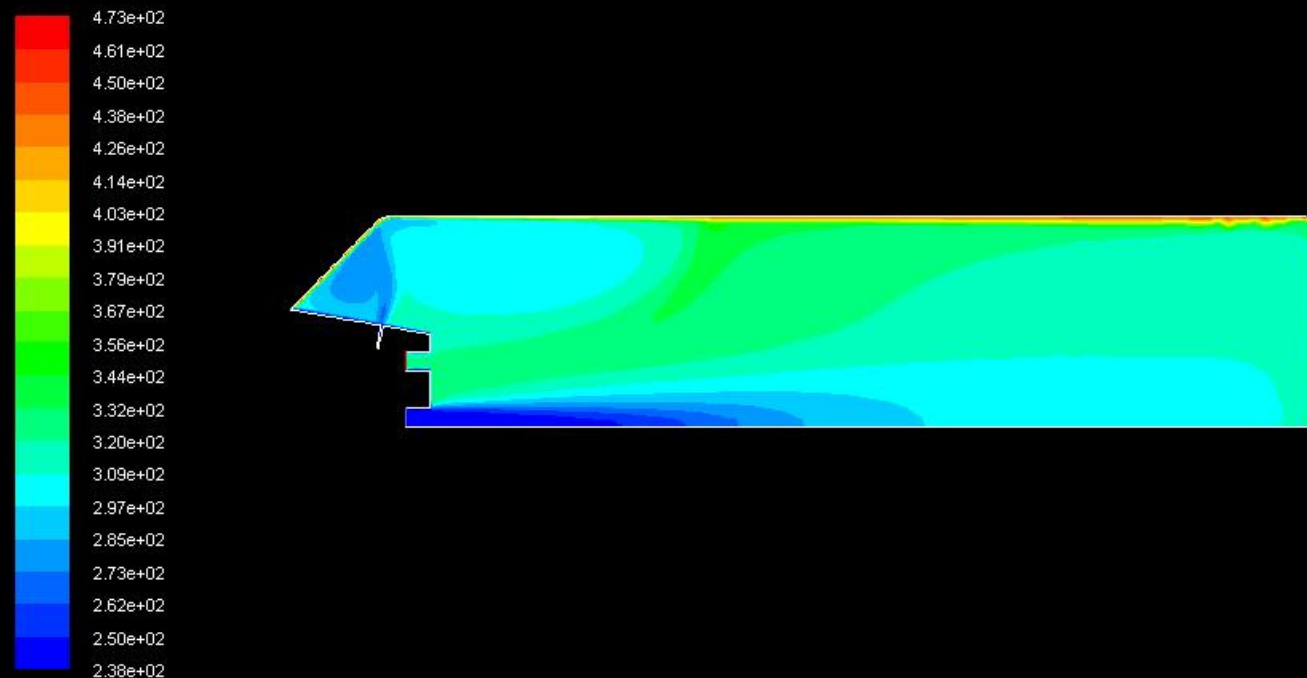
Vectorplot: around the thorn

Heat Flux on the wall

K- ϵ (realizable – Standard) K- ω (SST)

Static temperature -35°C

Temperatuur outlet: $47,3^{\circ}\text{C}$

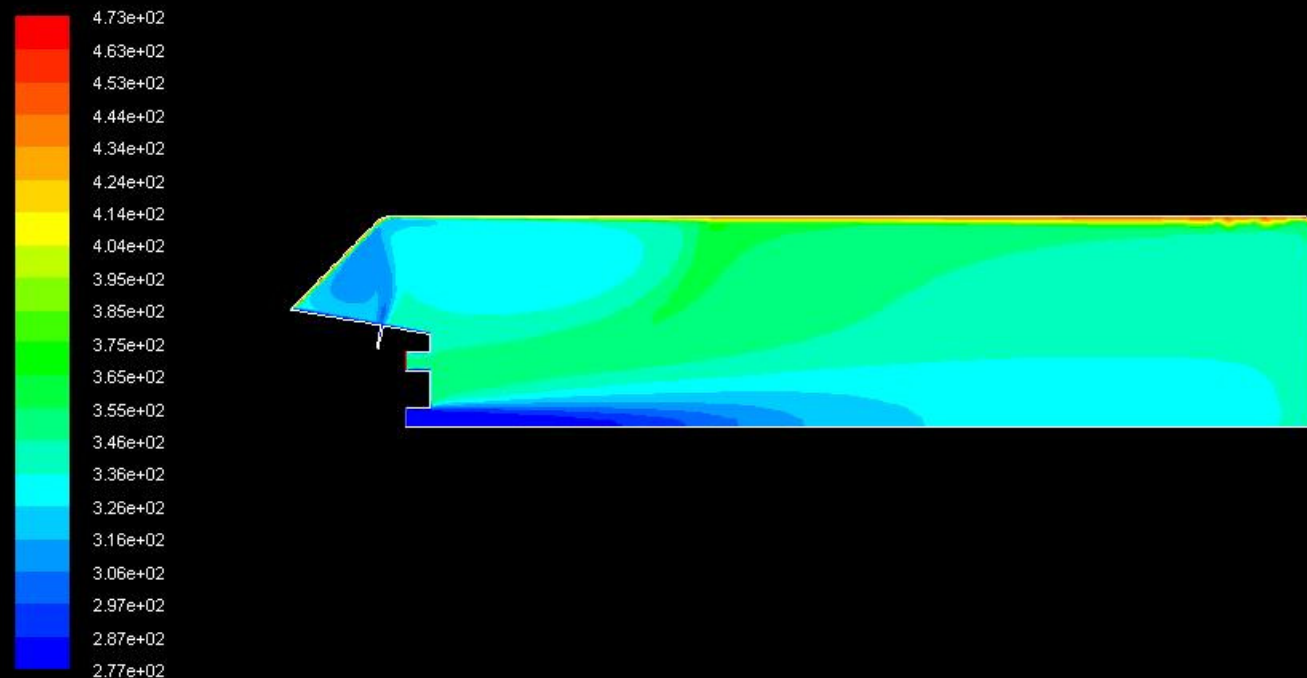


Contours of Static Temperature (K)

May 13, 2008
FLUENT 6.3 (axi, pbns, rke)

Static temperature 4 °C

Temperatuur outlet: 72,5 °C

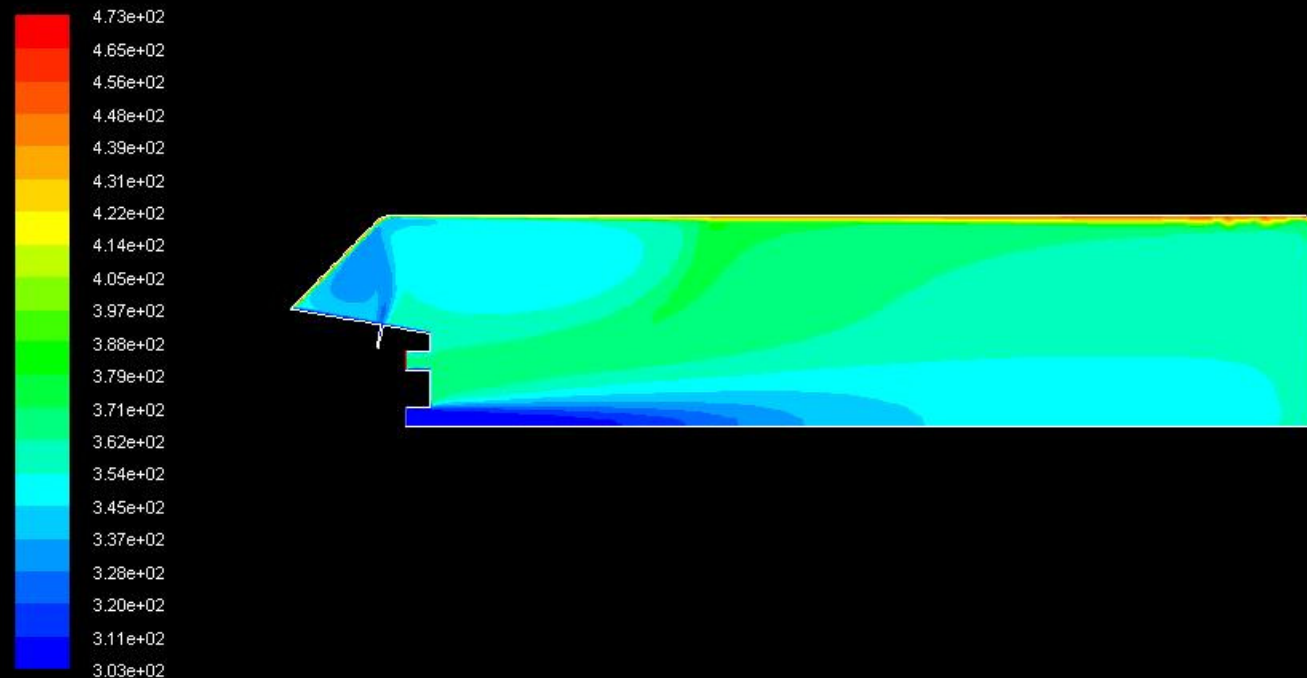


Contours of Static Temperature (K)

May 13, 2008
FLUENT 6.3 (axi, pbns, rke)

Static temperature 30 °C

Temperatuur outlet: 89,5 °C



Contours of Static Temperature (K)

May 13, 2008
FLUENT 6.3 (axi, pbns, rke)

Results

Temperature:

- At -35°C for the different flow rates
- At $0.0026\text{ m}^3/\text{s}$ on different temperatures

At largest flow rate, grid adaption is used in order to get correct Y^+ values)

(following is at $0.0026\text{ m}^3/\text{s}$ and -35°C Inlet temperature)

Contourplot

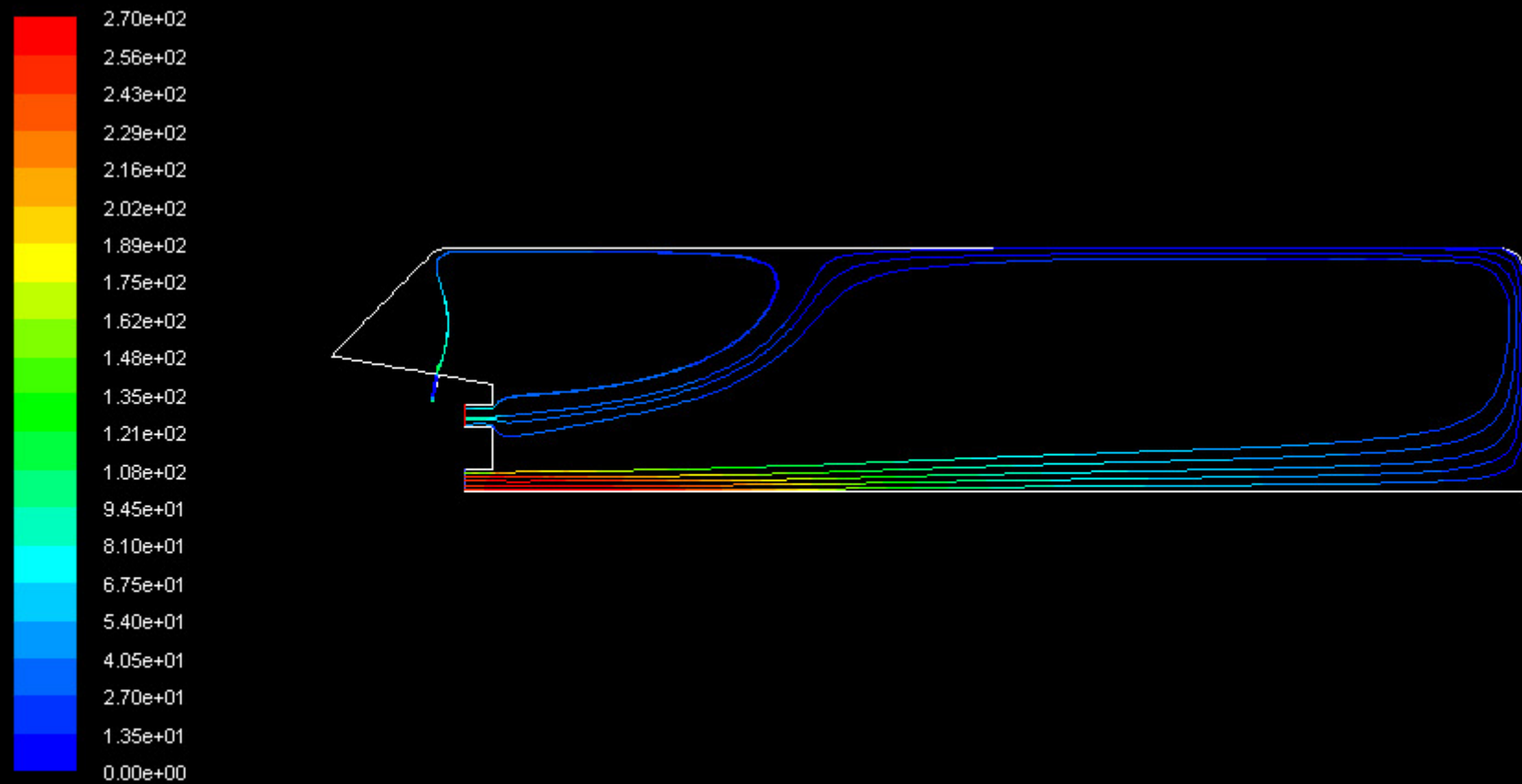
- Velocity magnitude \rightarrow flow rate almost no influence on path, only on magintude

Vectorplot: around the thorn

Heat Flux on the wall

K- ϵ (realizable – Standard) K- ω (SST)

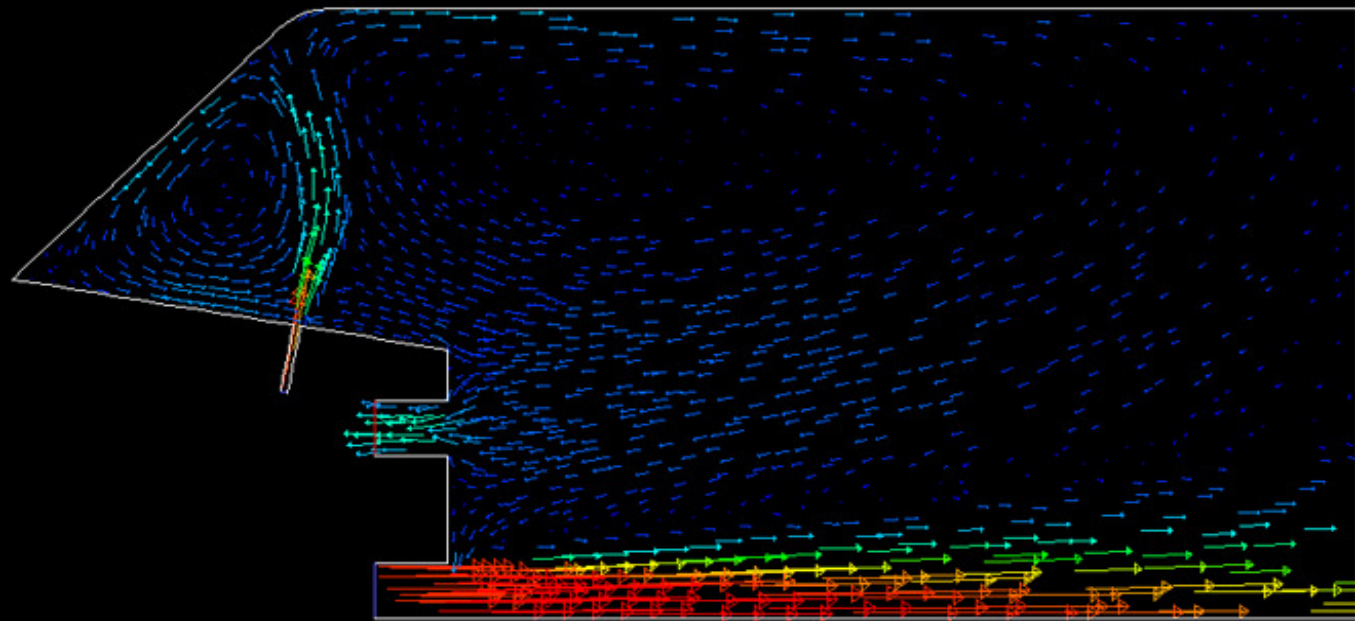
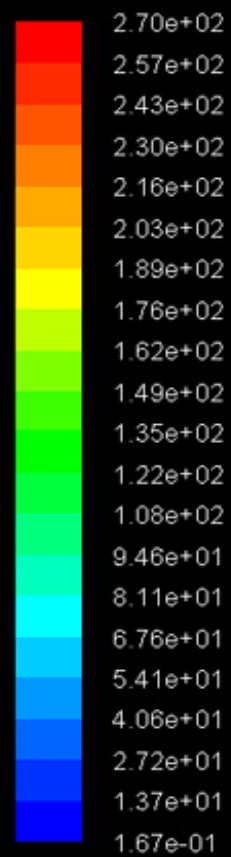
Pathlines



Pathlines Colored by Velocity Magnitude (m/s)

May 13, 2008
FLUENT 6.3 (axi, pbns, rke)

Vectorplot

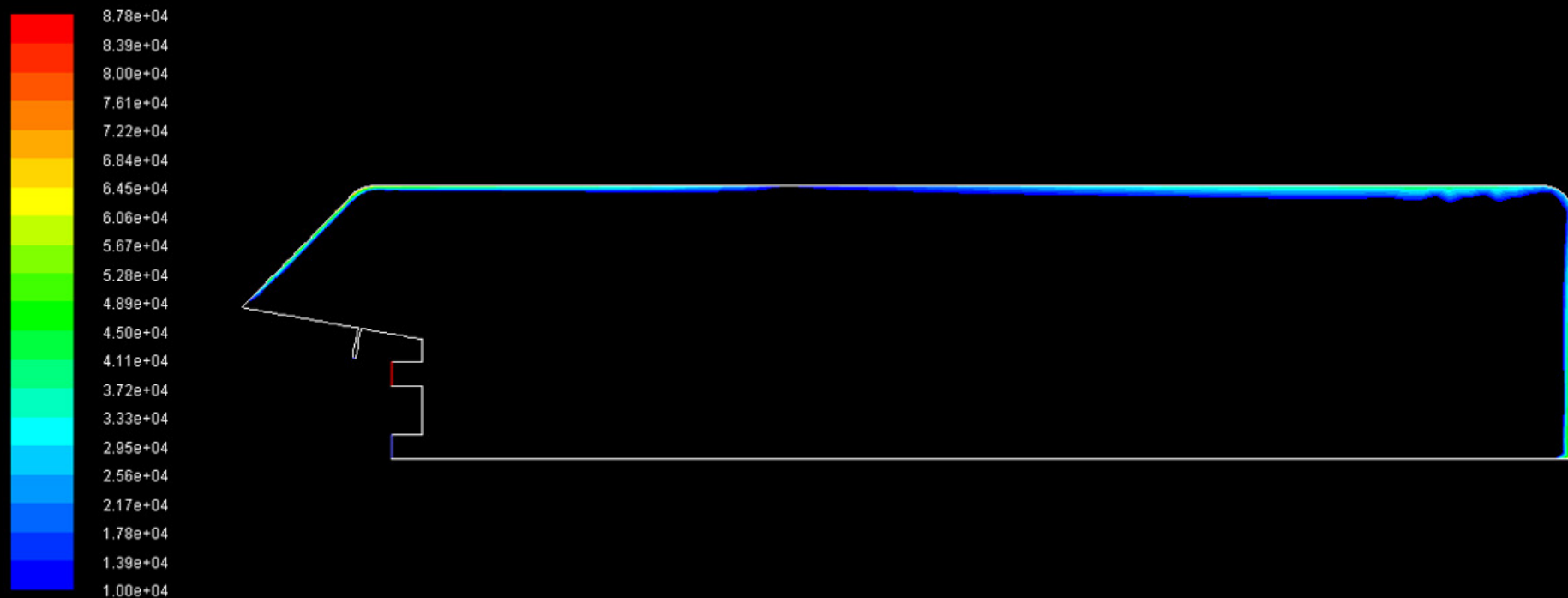


Velocity Vectors Colored By Velocity Magnitude (m/s)

May 15, 2008
FLUENT 6.3 (axi, pbns, rke)

Heat flux

Bij 0,026 m³/s en inlaattemperatuur –35 °C



Contours of Total Surface Heat Flux (w/m2)

May 15, 2008
FLUENT 6.3 (axi, pbns, rke)

Heat flux - Overview

Maximum values (situated at central of bottle base) in kW / m²

$T_{(°C)}$ \ $Q_{(m^3/s)}$	0,0065	0,013	0,026
-35	25,9	47,7	87,8
4	21,6	39,8	73,2
30	17,9	34,4	63,5

Results

Temperature:

- At -35°C for the different flow rates
- At $0.0026\text{ m}^3/\text{s}$ on different temperatures

At largest flow rate, grid adaption is used in order to get correct Y^+ values)

(following is at $0.0026\text{ m}^3/\text{s}$ and -35°C Inlet temperature)

Contourplot

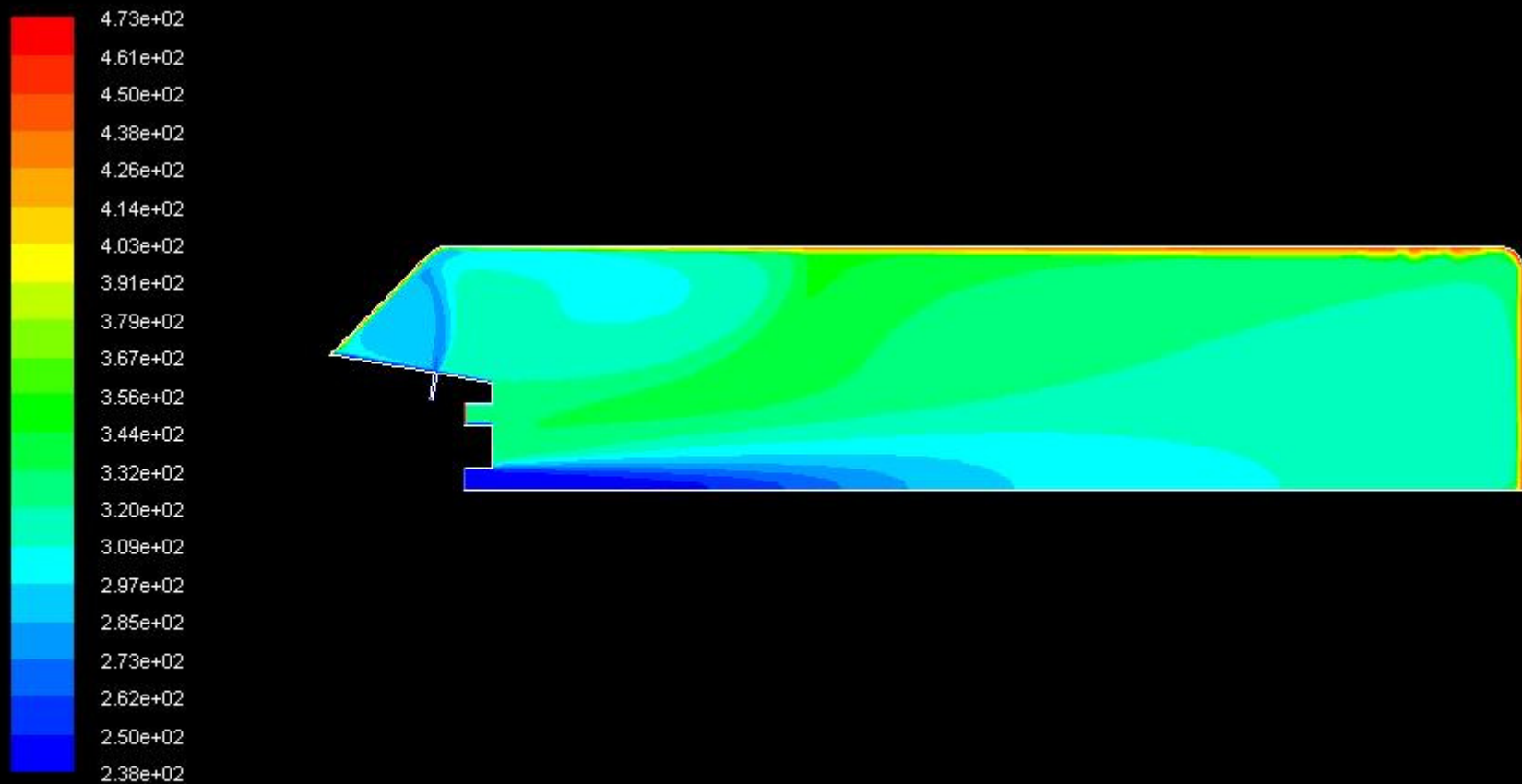
- Velocity magnitude \rightarrow flow rate almost no influence on path, only on magnitude

Vectorplot: around the thorn

Heat Flux on the wall

K- ϵ (realizable – Standard) K- ω (SST)

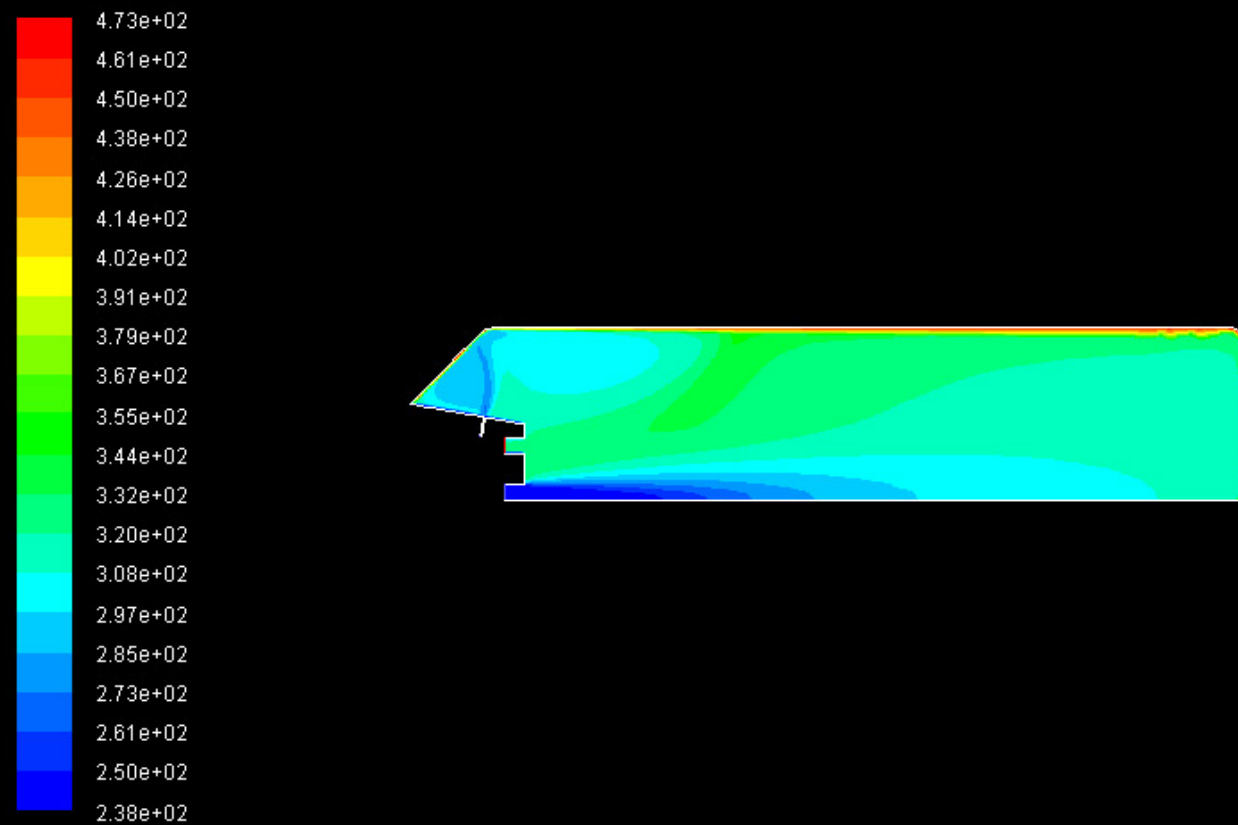
K-E realizable



Contours of Static Temperature (K)

May 13, 2008
FLUENT 6.3 (axi, pbns, rke)

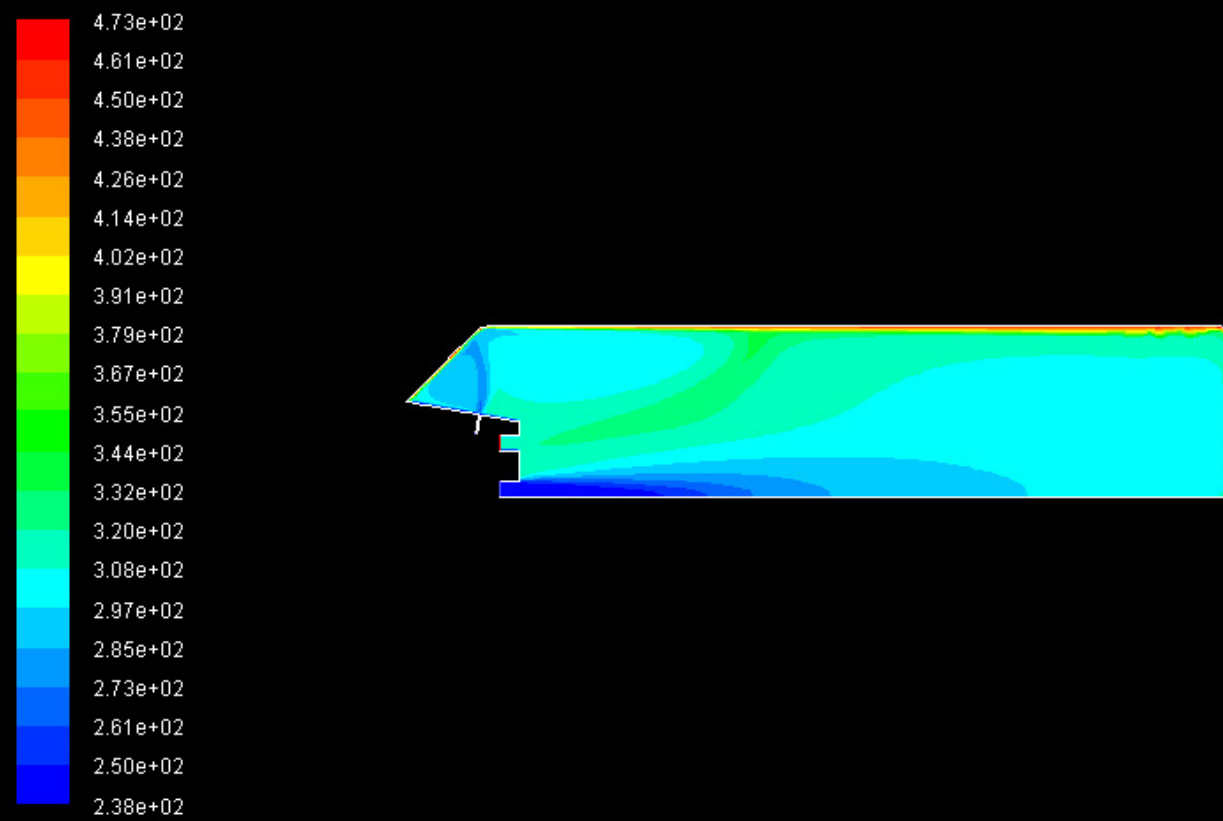
K-E Standard



Contours of Static Temperature (k)

May 14, 2008
FLUENT 6.3 (axi, pbns, ske)

K-W SST



Contours of Static Temperature (k)

May 14, 2008
FLUENT 6.3 (axi, pbns, sstk)